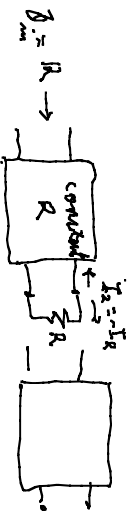


Partial pole removal circuit correction
Curve tracer libraries, bias

Constant R & grounding, bridged T
exp(A) from



$$\begin{aligned} \beta_{in} &= R \rightarrow \\ \beta_{in} &= \frac{V_1}{I_1} \Rightarrow \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} \beta_{11} & \beta_{12} \\ \beta_{21} & \beta_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} \\ & \quad -RI_2 \end{aligned}$$

$$\Rightarrow -RI_2 = \beta_{21}I_1 + \beta_{22}I_2$$

$$I_2 = (-R - \beta_{22})^{-1} \beta_{21} I_1$$

$$V_1 = \beta_{11}I_1 + \beta_{12} \left(\frac{-R - \beta_{22}}{R + \beta_{22}} \right) I_1 = RI_1 \text{ Constant } R$$

$$\beta_{11}R + \beta_{11}\beta_{22} - \beta_{12}\beta_{21} = R^2 + R\beta_{22}$$

$$\text{when } \beta_{22} = \beta_{11} \quad \beta_{11}R = \beta_{21}R \Rightarrow R^2 = \Delta_{\beta_1}$$

add a constant R lattice

constant R 2-port

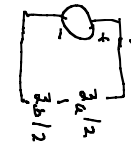
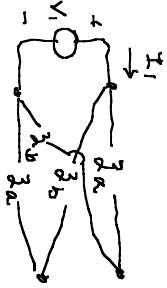


$$Z_{11} = \left. \frac{V_1}{I_1} \right|_{I_2=0}$$

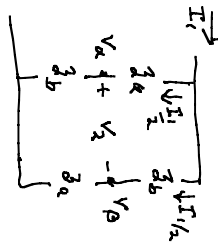
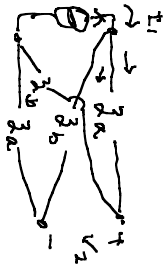
$$Z_{21} = \left. \frac{V_2}{I_1} \right|_{I_2=0}$$

derive Z matrix

$$Z_{11} = \left. \frac{V_1}{I_1} \right|_{I_2=0 \text{ (open)}}$$



$$V_1 = \frac{1}{2}(R_a + R_b) = Z_{11} = Z_{22}$$



$$V_2 = \frac{R_b}{R_b + R_a} I_1 = \frac{1}{2}(R_b - R_a) I_1$$

$$\left. \frac{V_2}{I_1} \right|_{I_2=0} = \frac{1}{2}(R_b - R_a)$$

$$Z = \frac{1}{2} \begin{bmatrix} R_a + R_b & R_b - R_a \\ R_b - R_a & R_b + R_a \end{bmatrix}$$

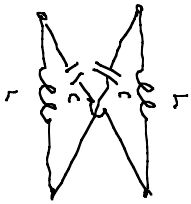
$$\Delta_3 = \frac{(R_a + R_b)^2}{4} - \frac{(R_b - R_a)^2}{4}$$

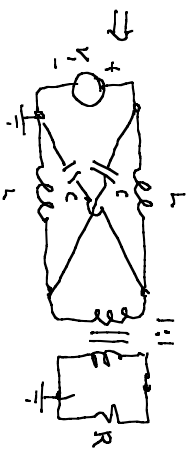
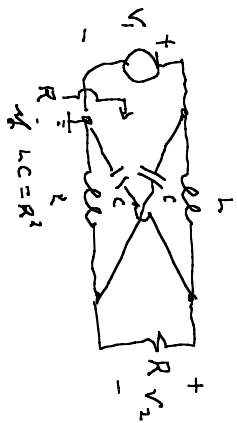
$$= \frac{(R_a^2 + 2R_a R_b + R_b^2) - (R_b^2 - 2R_b R_a + R_a^2)}{4} = R_a R_b$$

for constant R $\Delta_{KLM} R^2 = R_a R_b \Rightarrow \frac{R_b}{R_a} = \frac{R}{R_c}$

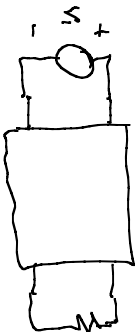
$$\frac{1}{R_c} = \frac{R^2}{R_a} \Rightarrow LC = R^2 \Rightarrow R = \sqrt{LC}$$

transfere von Formeln





allow output
input
provided



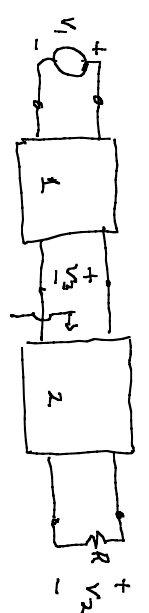
$$V_2 = R I_2 = Z_{21} I_1 + Z_{22} I_2$$

$$V_1 = Z_{11} I_1 + Z_{12} I_2 = R I_1$$

divide V_2
 V_1

$$I_1 = V_1/R \Rightarrow -R I_2 = Z_{21} \frac{V_1}{R} + Z_{22} I_2 \Rightarrow (-R - Z_{22}) I_2 = \frac{Z_{21}}{R} V_1 \Rightarrow I_2 = \frac{Z_{21}}{R} \frac{-1}{R + Z_{22}} V_1$$

$$V_2 = -R I_2 = -R \left(\frac{-Z_{21}}{R(R + Z_{22})} \right) V_1 \Rightarrow \frac{V_2}{V_1} = \frac{Z_{21}}{R + Z_{22}} = \frac{\frac{1}{2}(Z_o - Z_a)}{R + \frac{1}{2}(Z_o + Z_a)} = \frac{Z_o - Z_a}{Z_o + 2R + Z_a} = A_v$$



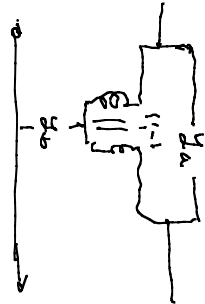
$$\frac{V_3}{V_1} \cdot \frac{V_2}{V_3} = A_{v1} \cdot A_{v2}$$

load is R

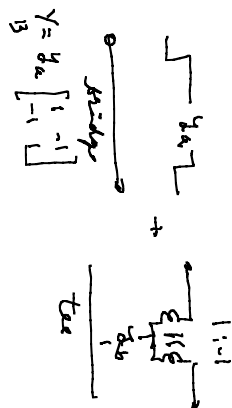
\therefore constant R between multiply
gain; stable if Z_a, Z_o are PR or RDR

$$A_v = \frac{Z_o - Z_a}{R + Z_o} = \frac{\frac{3b/R - 3a}{3b/R + 2R + 3a}}{\frac{3b/R + 2R + 3a}{3b/R + 2R + 3a}} = \frac{1 - (3a/R)^2}{(3a/R)^2 + 2(3a/R) + 1} = \frac{(1 - (3a/R)^2)^2}{(1 + (3a/R))^2}$$

Look at constant with a common ground

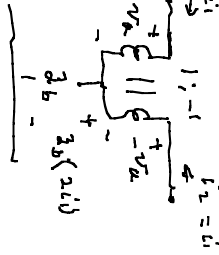


⇒ add admittance



$$\Rightarrow Y \Rightarrow \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \frac{1}{4z_b} \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$\Rightarrow Y_c = \frac{1}{4z_b} \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$$



$$v_1 = v_a + z_b(i_1)$$

$$v_2 = -v_a + z_b(2i_1)$$

$$v_1 + v_2 = 4z_b \cdot i_1$$

$$Y = \begin{bmatrix} \frac{y_b}{4} & -\frac{y_a}{4} \\ \frac{y_b}{4} & -\frac{y_a}{4} \end{bmatrix}$$

$$= \frac{1}{2} \begin{bmatrix} \frac{y_b + z_a}{2} & \frac{y_b - z_a}{2} \\ \frac{y_b - z_a}{2} & \frac{y_b + z_a}{2} \end{bmatrix}$$

$$= \frac{1}{2} \begin{bmatrix} Y_a + Y_b & Y_a - Y_b \\ Y_a - Y_b & Y_a + Y_b \end{bmatrix}$$

∴ a constant matrix

as Y matrices appear

$$Z = \frac{1}{2} \begin{bmatrix} z_b + z_a & z_b - z_a \\ z_b - z_a & z_b + z_a \end{bmatrix}$$

$$Y = \frac{1}{2} \begin{bmatrix} \frac{y_b + z_a}{2} & \frac{y_b - z_a}{2} \\ \frac{y_b - z_a}{2} & \frac{y_b + z_a}{2} \end{bmatrix}$$

constant matrix